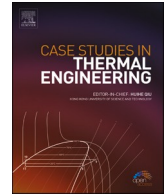




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Fractional order simulations for the thermal determination of graphene oxide (GO) and molybdenum disulphide (MoS_2) nanoparticles with slip effects

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ABSTRACT

In this thermal investigation, the mixed free convection Casson nanofluid along with heat transfer effects over a vertical plate is addressed. The thermal radiative phenomenon is also considered to improve the heat transfer rate. For base fluid, the engine oil is assumed for which the thermal enhancement is predicted with the suspension of graphene oxide (GO) and molybdenum disulphide (MoS_2) nanoparticles. To construct the fractional model, the partial derivative with respect to time is exchanged by the recent definitions of fractional derivatives namely Atangana-Baleanu (AB) and Caputo-Fabrizio (CF) time-fractional derivative and the Laplace scheme is applied to obtain the solution of governing equations. To enhance the innovation of this article different cases of velocity profiles are examined. The effects of different parameters are examined graphically and numerically by varying the values of parameters. The reported results claimed that the simulations performed via AB-time fractional are more stable as compared to the Caputo-Fabrizio time-fractional approach. The velocity profile declines with increasing the fractional parameters while increasing change in velocity has been observed for Grashof number. The nanoparticles temperature shows a lower change due to volume fraction coefficient.

1. Introduction

Following to the remarkable thermophysical aspects and stable features, the nanofluids offer well reputed applications in industrial and engineering sectors. The nano-materials attained ultra-high and fascinating features like viscosity, thermal conductivity and surface tension in contrast to the base materials. The inclusion of nanoparticles and base fluids improves the thermal capability of base liquids more precisely. The lack of energy resources and challenging pronounced the industrial and engineering products as many of such phenomenon involves the base fluid as an energy source. This substantial issue is solved by utilizing the nanoparticles as an

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Nomenclatures

w	Velocity[m /s]
t	Time[s]
U_o	Constant Velocity[m /s]
ρ_{nf}	Density ofnanofluid[Kg /m ³]
T	Non-Dimensional temperature[K]
k_{nf}	Thermal conductivity of nanofluid[W /m ² k]
Pr	Prandtl number
Gr	Grashof number
β_c	Casson parameter
μ_{nf}	Dynamic viscosity off nanofluid [Kg /ms]
ρ_s	Density of nanoparticles[Kg /m ³]
β	AB-fractional derivative operator
α	CF-fractional derivative operator
Nu	Nusselt number
C_f	Skin Friction
CF	Caputo-Fabrizio fractional derivative
β	AB-fractional parameter
q	Laplace variable by AB
s	Laplace variable by CF
g	Acceleration due to gravity[m /s ²]
AB	Atangana-Baleanu fractional derivative
ρ_f	Density of base fluid[Kg /m ³]

energy source with immersion with base fluids. Choi [1] pronounced the basic features of nanoparticles via experimental support. Siddiqui and Turkyilmazoglu [2] followed a theoretical continuation for inspecting the ferro-nanoparticles thermal prospective confined by cavity. Abbas et al. [3] worked out the hybrid nano-material flow model induced via nonlinear cylinder. Nadeem et al. [4] simulated a dual simulations fo a nanofluid problem accounted with anisotropic slip features. Khan et al. [5] explained the thermal outcomes of couple stress nanofluid subject to the slip mechanism. The viscoelastic nanofluid properties with modified porous space law with convective conditions were identified by Waqas et al. [6]. Kumar et al. [7] determined the nanofluid applications with KKL correlations over a moving curved surface with implementation of shooting technique. Khan et al. [8] visualized the modified second grade nanoparticles flow with prescribed features of nonlinear thermal radiation. Mandal and Shit [9] presented the entropy generation investigation for the biviscosity nanofluid over rotating permeable disk. The interesting numerical model for the hybrid nanoparticles over spinning disk was claimed by Acharya [10]. Zhang et al. [11] observed the thermal upshot for gold and silver nanoparticles subject to the melting applications. The 3-D nanoparticles analysis for the radiative flow of Jeffrey nanofluid was analytically worked out by Ahmad et al. [12]. Vaidya et al. [13] determined the Riga nanofluid flow with mixed convection analysis. Pourhoseini et al. [14] experimentally noticed the inclusion of Al₂O₃ nanoparticles with biodiesel base liquid results improved thermal features. Hassan et al. [15] addressed the thermal applications of hybrid nanofluid with experimental justifications. Gowda et al. [16] presented the role of slip features in the Casson-Maxwell nanofluid via stretching disks. Jamshed et al. [17] followed the single phase nanofluid model to address the thermal aspects of second grade nanofluid with radiative phenomenon. Gowda et al. [18] inspected the influence of magnetic dipole for ferromagnetic nanoparticles flow in presence of Stefan blowing constraints. Kumar et al. [19] reported the dusty fluid thermal enhancement in presence of hybrid nanoparticles confined by stretched cylinder. The computation analysis for the nanoparticles flow by following the Koo–Kleinstreuer and Li (KKL) model was identified by Gowda et al. [20].

The fractional calculus is the interesting branch of mathematics which is associated to the derivative and integrals of various types. The significant interest of researchers is developed on this topic in last some years. Different definitions of fractional derivatives with local and non-local approach are developed. The implementations of non-local derivative are more precise able due to involved function. A new types of fractional derivative is Atangana-Baleanu (AB) derivative which solved the local kernel for the Caputo-Fabrizio (CF) derivative. Many authors followed this approach to discuss the fractional simulations for various problems [21–32].

After claiming the improved thermal upshot of nanoparticles, this contribution reflects the thermal enhancement of graphene oxide (GO) and molybdenum disulphide (MoS₂) nanoparticles over vertically moving plate with help of fractional approach. The Casson liquid is assumed to be base fluid. The Casson fluid characterizes the properties of shear thinning more effectively [33–35]. Literature regarding new developments in fluid flow in view of different fluid model is listed in Refs. [36–40]. The characteristics of base fluid are referred to the engine oil applications. The fractional simulations for the formulated problem are performed with help of Atangana-Baleanu (AB) and Caputo-Fabrizio (CF) time-fractional derivative. The solution for momentum and thermal boundary layer via fractional simulations is presented. The special case for the flow motion is also considered.

2. Problem formulation

The vertical plate flow of Casson fluid has been considered Casson fluid with immersion of graphene oxide (GO) and molybdenum disulphide (MoS₂) nanoparticles. In start of simulations, (t = 0), the temperature is kept constant according to the atmosphere. After some time t = 0⁺, the stationary plate starts to vibrate with constant velocity $\frac{f(t)}{\mu}$ and temperature varies to ϑ_w . Here, f(t) is a non-negative function with f(0) = 0 and having some of its Laplace transformations and also supposed that the slip exists on the boundaries of the wall and the velocity at the bottom is proportional to shear stress. With the vibration of the plate, fluid also starts to flow on the vibrating plate with the same velocity as the plate oscillates. The governing equations representing the flow of Casson fluid with nanoparticles are [26,27,33]:

$$\rho_{nf} \frac{\partial w(\xi, t)}{\partial t} = \mu_{nf} \left(1 + \frac{1}{v} \right) \frac{\partial^2 w(\xi, t)}{\partial \xi^2} + g(\rho\beta)_{nf} [\vartheta(\xi, t) - \vartheta_\infty] ; \quad \xi, t > 0 \tag{1}$$

$$(\rho C_p)_{nf} \frac{\partial \vartheta(\xi, t)}{\partial t} = k_{nf} \frac{\partial^2 \vartheta(\xi, t)}{\partial \xi^2} ; \quad \xi, t > 0 \tag{2}$$

With proper its respective conditions:

$$w(\xi, 0) = 0, \quad \vartheta(\xi, 0) = \vartheta_\infty \quad ; \quad \xi > 0 \tag{3}$$

$$w(\xi, t) - b \frac{\partial w(\xi, t)}{\partial \xi} = \frac{f(t)}{\mu}, \quad \frac{\partial \vartheta(\xi, t)}{\partial \xi} = -\frac{h}{k} \vartheta(\xi, t) ; \quad \xi = 0, t > 0 \tag{4}$$

$$w(\xi, t) \rightarrow 0, \quad \vartheta(\xi, t) \rightarrow 0 ; \quad \xi \rightarrow \infty, t > 0 \tag{5}$$

where

$$\begin{aligned} \mu_{nf} &= \frac{\mu_f}{(1 - \phi)^{2.5}}, \quad \rho_{nf} = (1 - \phi)\rho_f + \phi\rho_s \\ (\rho\beta)_{nf} &= (1 - \phi)(\rho\beta)_f + \phi(\rho\beta)_s, \quad (\rho C_p)_{nf} = (1 - \phi)(\rho C_p)_f + \phi(\rho C_p)_s \\ \frac{k_{nf}}{k_f} &= \frac{k_s + 2k_f - 2\phi(k_f - k_s)}{k_s + 2k_f + \phi(k_f - k_s)}, \quad \frac{\sigma_{nf}}{\sigma_f} = \frac{\sigma_s + 2\sigma_f - 2\phi(\sigma_f - \sigma_s)}{\sigma_s + 2\sigma_f + \phi(\sigma_f - \sigma_s)} \end{aligned}$$

are the dynamic viscosity, the effective density of the nanofluid, heat capacitance, thermal conductivity, electrical conductivity of the engine oil-based nanofluids. The thermal properties of engine oil, graphene oxide (GO) and molybdenum disulphide (MoS₂) nanoparticles are presented in Table 1.

Now to non-dimensionalize the respective governing equations and conditions, introducing the appropriate non-dimensional parameters as follows:

$$w^* = \frac{w}{U_o}, \quad \xi^* = \frac{\xi U_o}{v_f}, \quad b^* = \frac{b U_o^2}{v}, \quad t^* = \frac{t U_o^2}{v_f}, \quad T^* = \frac{\vartheta - \vartheta_\infty}{\vartheta_w - \vartheta_\infty}, \quad f^*(t^*) = \frac{1}{\mu} \sqrt{\frac{t_o}{v'}} f(t_o t^*)$$

After the process of non-dimensionalization, we yield the subsequent governing equations and conditions

$$\left((1 - \phi)\rho_f + \phi \frac{\rho_s}{\rho_f} \right) \frac{\partial w(\xi, t)}{\partial t} = \frac{1}{(1 - \phi)^{2.5}} \left(1 + \frac{1}{v} \right) \frac{\partial^2 w(\xi, t)}{\partial \xi^2} + \left((1 - \phi) + \phi \frac{(\rho\beta)_s}{(\rho\beta)_f} \right) Gr T(\xi, t) ; \quad \xi, t > 0 \tag{6}$$

$$\left((1 - \phi) + \phi \frac{(\rho C_p)_s}{(\rho C_p)_f} \right) Pr \frac{\partial T(\xi, t)}{\partial t} = \frac{k_{nf}}{k_f} \frac{\partial^2 T(\xi, t)}{\partial \xi^2} ; \quad \xi, t > 0 \tag{7}$$

with

$$w(\xi, 0) = 0, \quad T(\xi, 0) = 0 \quad ; \quad \xi > 0 \tag{8}$$

Table 1
Physical properties of engine oil and nanoparticles [25].

Material	ρ (Kg /m ³)	C_p (J /Kg K)	k (w /m.K)	$\beta \times 10^5$ (1 /K)
Engine Oil	884	1910	0.144	70
GO	1800	717	5000	0.284
MoS ₂	5060	397.21	904.4	2.8424

$$w(\xi, t) - b \frac{\partial w(\xi, t)}{\partial \xi} = f(t), \quad \frac{\partial T(\xi, t)}{\partial \xi} = -(1 + T(\xi, t)) \quad ; \quad \xi = 0, t > 0 \tag{9}$$

$$w(\xi, t) \rightarrow 0, T(\xi, t) \rightarrow 0; \xi \rightarrow \infty, t > 0 \tag{10}$$

Preliminaries: To construct the fractional model recent definitions of fractional derivatives namely AB and CF-time fractional derivative are utilized, whose mathematical form is defined as [26] for the function $f(\xi, t)$

$${}^{AB}\mathcal{D}_t^\beta f(\xi, t) = \frac{1}{1-\beta} \int_0^t E_\beta \left[\frac{\beta(t-z)^\beta}{1-\beta} \right] f'_{(\xi,t)} dt \tag{11}$$

with its Laplace transformation [27].

$$\mathcal{L}\left\{{}^{AB}\mathcal{D}_t^\beta f(\xi, t)\right\} = \frac{q^\beta \mathcal{L}[f(\xi, t)] - q^{\beta-1} f(\xi, 0)}{(1-\beta)q^\beta + \beta} \tag{12}$$

The mathematical definition of CF-time fractional derivative for the function $f(\xi, t)$ is

$${}^{CF}\mathcal{D}_t^\alpha f(\xi, t) = \frac{1}{1-\alpha} \int_0^t \exp\left(\frac{\alpha(1-\tau)}{1-\alpha}\right) f'(\xi, t) d\tau \tag{13}$$

With its Laplace as [28,29]:

$$\mathcal{L}\left\{{}^{CF}\mathcal{D}_t^\alpha f(\xi, t)\right\} = \frac{s\mathcal{L}[f(\xi, t)] - f(\xi, 0)}{(1-\alpha)s + \alpha} \tag{14}$$

3. Modeling with AB-time fractional derivative

The fraction modal with the definition of AB-fractional derivative (11) can be formulated by replacing the partial derivative w.r.t time of transformed equations (6) and (7) by ${}^{AB}\mathcal{D}_t^\beta$ which is the operator of AB-fractional derivative

$$\Lambda_1 {}^{AB}\mathcal{D}_t^\beta w(\xi, t) = \Lambda_2 \beta_c \frac{\partial^2 w(\xi, t)}{\partial \xi^2} + \Lambda_3 GrT(\xi, t), \tag{15}$$

$$\Lambda_4 Pr {}^{AB}\mathcal{D}_t^\beta T(\xi, t) = \Lambda_5 \frac{\partial^2 T(\xi, t)}{\partial \xi^2}, \tag{16}$$

where

$$\Lambda_1 = (1-\phi)\rho_f + \phi \frac{\rho_s}{\rho_f}, \quad \Lambda_2 = \frac{1}{(1-\phi)^{2.5}}, \quad \Lambda_3 = (1-\phi) + \phi \frac{(\rho\beta)_s}{(\rho\beta)_f}$$

$$\Lambda_4 = (1-\phi) + \phi \frac{(\rho C_p)_s}{(\rho C_p)_f}, \quad \Lambda_5 = \frac{k_{nf}}{k_f}, \quad \beta_c = 1 + \frac{1}{v}$$

3.1. Energy equation via AB-fractional derivative

By applying the Laplace definition on AB-fractional model equation (16) for the solution of energy equation and on its corresponding conditions

$$\Lambda_4 Pr \left(\frac{q^\beta \mathcal{L}[T(\xi, t)] - q^{\beta-1} T(\xi, 0)}{(1-\beta)q^\beta + \beta} \right) = \Lambda_5 \frac{\partial^2 \bar{T}(\xi, q)}{\partial \xi^2}, \tag{17}$$

Where $\bar{T}(\xi, q)$ is the Laplace of $T(\xi, t)$, with respective conditions

$$\left. \frac{\partial \bar{T}}{\partial \xi} \right|_{\xi=0} = - \left(\frac{1}{q} + \bar{T}(0, q) \right), \quad \bar{T}(\xi, q) \rightarrow 0 \text{ as } \xi \rightarrow \infty.$$

By introducing the above conditions, the solution of the energy equation will be

$$\bar{T}(\xi, q) = \frac{1}{\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}} - 1\right)} \frac{e^{-\xi \sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}}}{q} \tag{18}$$

The Laplace inverse of equation (18) will be analyzed numerically by Stehfest and Zakians methods in Table 2.

3.1.1. Momentum equation via AB-fractional derivative

For the solution of the momentum equation, applying the Laplace transformation on equation (15) and its respective transformed boundary conditions.

$$\Lambda_1 \left(\frac{q^\beta \mathcal{L}[w(\xi, t)] - q^{\beta-1} w(\xi, 0)}{(1-\beta)q^\beta + \beta} \right) = \Lambda_2 \beta_c \frac{\partial^2 \bar{w}(\xi, q)}{\partial \xi^2} + \Lambda_3 Gr \bar{T}(\xi, q), \tag{19}$$

with:

$$\begin{aligned} \bar{w}(\xi, q) - b \frac{\partial \bar{w}(\xi, q)}{\partial \xi} &= F(q) \text{ as } \xi = 0, \\ \bar{w}(\xi, q) &\rightarrow 0 \text{ as } \xi \rightarrow \infty. \end{aligned} \tag{20}$$

Simplifying equation (19) and using the above conditions we yield the solution of the momentum equation as follows

$$\begin{aligned} \bar{w}(\xi, q) &= \frac{1}{1 + b \sqrt{\frac{\Lambda_1}{\Lambda_2 \beta_c} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2 \beta_c} \frac{1}{q \left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}} - 1 \right)} \frac{1 + b \sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2 \beta_c} \right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta + \beta} \right)} + F(q) \right) e^{-\xi \sqrt{\frac{\Lambda_1}{\Lambda_2 \beta_c} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}} \\ &\quad - \frac{\Lambda_3 Gr}{\Lambda_2 \beta_c} \frac{1}{q \left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}} - 1 \right) \left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2 \beta_c} \right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta + \beta} \right)} e^{-\xi \sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}} \end{aligned} \tag{21}$$

4. Modeling with CF-time fractional derivative

For the fractional model of CF-time fractional derivative replacing the partial derivative w.r.t time by CF-fractional operator ${}^{CF} \mathcal{D}_t^\alpha$, we obtain the following governing equations

$$\Lambda_1 {}^{CF} \mathcal{D}_t^\alpha w(\xi, t) = \Lambda_2 \beta_c \frac{\partial^2 w(\xi, t)}{\partial \xi^2} + \Lambda_3 Gr T(\xi, t) \tag{22}$$

$$\Lambda_4 Pr {}^{CF} \mathcal{D}_t^\alpha T(\xi, t) = \Lambda_5 \frac{\partial^2 T(\xi, t)}{\partial \xi^2}; \xi, t > 0 \tag{23}$$

With transformed conditions

$$\begin{aligned} w(\xi, 0) &= 0, \quad T(\xi, 0) = 0 \quad ; \quad \xi > 0 \\ w(\xi, t) - b \frac{\partial w(\xi, t)}{\partial \xi} &= f(t), \quad \left. \frac{\partial T}{\partial \xi} \right|_{\xi=0} = -(1 + T(0, t)); \quad \xi = 0, t > 0 \end{aligned}$$

Table 2
Analysis of temperature and Nusselt number with the variation in fractional parameter.

α, β	Temp (AB)	Temp (CF)	Nu (AB)	Nu (CF)
0.1	0.6076	0.6055	2.4256	2.5573
0.2	0.5986	0.5905	2.4821	2.6739
0.3	0.5784	0.5620	2.5691	2.7777
0.4	0.5455	0.5199	2.6776	2.8701
0.5	0.5006	0.4664	2.7961	2.9521
0.6	0.4459	0.4047	2.9129	3.0249
0.7	0.3843	0.3381	3.0177	3.0890
0.8	0.3180	0.2688	3.1033	3.1447
0.9	0.2486	0.1982	3.1656	3.1924

$$w(\xi, t) \rightarrow 0, \quad T(\xi, t) \rightarrow 0 \quad ; \quad \xi \rightarrow \infty, \quad t > 0$$

4.1. Energy equation via CF-fractional derivative

As the energy equation (23) is independent of momentum profile so by applying the Laplace on equation (23)

$$\Lambda_4 Pr \left(\frac{s \mathcal{L}[T(\xi, t)] - T(\xi, 0)}{(1-\alpha)s + \alpha} \right) = \Lambda_5 \frac{\partial^2 \bar{T}(\xi, s)}{\partial \xi^2} \tag{24}$$

where $\bar{T}(\xi, s)$ is the Laplace of $T(\xi, t)$, with the following transformed conditions:

$$\left. \frac{\partial \bar{T}}{\partial \xi} \right|_{\xi=0} = - \left(\frac{1}{s} + \bar{T}(0, s) \right), \quad \bar{T}(\xi, s) \rightarrow 0 \text{ as } \xi \rightarrow \infty$$

By utilizing these conditions, we attained the solution of temperature distribution as

$$\bar{T}(\xi, s) = \frac{1}{s \left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}} - 1 \right)} e^{-\xi \sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}}} \tag{25}$$

The inverse of Laplace of Eq. (25) will be shortened numerically in Table 2.

4.2. Momentum equation via CF-fractional derivative

Eq. (22) is a partial differential equation of CF-time fractional modal, so utilizing the Laplace transformation on equation (22), we get

$$\Lambda_1 \left(\frac{s \mathcal{L}[w(\xi, t)] - w(\xi, 0)}{(1-\alpha)s + \alpha} \right) = \Lambda_2 \beta_c \frac{\partial^2 \bar{w}(\xi, s)}{\partial \xi^2} + \Lambda_3 Gr \bar{T}(\xi, s) \tag{26}$$

With the following transformed conditions

$$\bar{w}(\xi, s) - b \frac{\partial \bar{w}(\xi, s)}{\partial \xi} = F(s) \text{ as } \xi = 0$$

$$\bar{w}(\xi, s) \rightarrow 0 \text{ as } \xi \rightarrow \infty \tag{27}$$

The following solution of Eq. (26) can be accomplished by exploiting the above condition (27)

$$\bar{w}(\xi, s) = \frac{1}{1 + b \sqrt{\frac{\Lambda_1}{\Lambda_2 \beta_c} \frac{s}{(1-\alpha)s + \alpha}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2 \beta_c} \frac{1}{s \left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}} - 1 \right)} \frac{1 + b \sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2 \beta_c} \right) \left(\frac{s}{(1-\alpha)s + \alpha} \right)} + F(s) \right) e^{-\xi \sqrt{\frac{\Lambda_1}{\Lambda_2 \beta_c} \frac{s}{(1-\alpha)s + \alpha}}} - \frac{\Lambda_3 Gr}{\Lambda_2 \beta_c} \frac{1}{s \left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}} - 1 \right)} \frac{e^{-\xi \sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2 \beta_c} \right) \left(\frac{s}{(1-\alpha)s + \alpha} \right)} \tag{28}$$

For the inverse of Laplace of the velocity field via AB and CF-fractional derivative of Eqs. (21) and (28) respectively, we will use the numerical methods i.e. Grave Stehfest and Zakians method [30–32]:

$$w(\xi, t) = \frac{\ln(2)}{t} \sum_{n=1}^M v_n \bar{w} \left(\xi, n \frac{\ln(2)}{t} \right)$$

where M will be a positive integer. Moreover:

$$v_n = (-1)^{n+\frac{M}{2}} \sum_{p=\frac{q-1}{2}}^{\min\left(q, \frac{M}{2}\right)} \frac{p^{\frac{M}{2}}(2p)!}{\left(\frac{M}{2}-p\right)!p!(p-1)!(q-p)!(2p-q)!}$$

and

$$w(\xi, t) = \frac{2}{t} \sum_{j=1}^N Re\left(k_j \cdot \bar{w}\left(\xi, \frac{\alpha_j}{t}\right)\right)$$

are the Stehfest and Zaki's methods respectively.

4.2.1. Special cases

As the solution of momentum field via AB and CF-fractional derivative in Eqs. (21) and (28) respectively, are in a more general form. Therefore, to illustrate some more physical insight into the problem, here we will discuss some special cases for the function $f(t)$. So here we will discuss some special cases for the velocity profile in the ramped wall case whose physical interpretation is well known in the literature.

Case 1. $f(t) = t$

In the first case, take $f(t) = t$ then the expressions of velocity field by AB and CF-fractional derivative with Eqs. (21) and (28) respectively will become as

$$\begin{aligned} \bar{w}(\xi, q) = & \frac{1}{1 + b\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}} - 1\right)} \frac{1 + b\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c}\right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta + \beta}\right)} + \frac{1}{q^2} \right) e^{-\xi\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}} \\ & - \frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}} - 1\right) \left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c}\right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta + \beta}\right)} e^{-\xi\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}} \end{aligned} \tag{29}$$

and

$$\begin{aligned} \bar{w}(\xi, s) = & \frac{1}{1 + b\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{s}{(1-\alpha)s + \alpha}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{s\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}} - 1\right)} \frac{1 + b\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c}\right) \left(\frac{s}{(1-\alpha)s + \alpha}\right)} + \frac{1}{s^2} \right) e^{-\xi\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{s}{(1-\alpha)s + \alpha}}} \\ & - \frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{s\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}} - 1\right) \left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c}\right) \left(\frac{s}{(1-\alpha)s + \alpha}\right)} e^{-\xi\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s + \alpha}}} \end{aligned} \tag{30}$$

Case 2. $f(t) = \text{Sin}(\omega t)$

In the second case, take $(t) = \text{Sin}(t)$ where ω represents the strength of the shear stress, then the expressions of velocity field by AB and CF-fractional derivative with Eqs. (21) and (28) become:

$$\begin{aligned} \bar{w}(\xi, q) = & \frac{1}{1 + b\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}} - 1\right)} \frac{1 + b\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c}\right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta + \beta}\right)} + \frac{\omega}{\omega^2 + q^2} \right) e^{-\xi\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}} \\ & - \frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}} - 1\right) \left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c}\right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta + \beta}\right)} e^{-\xi\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta + \beta}}} \end{aligned} \tag{31}$$

and

$$\bar{w}(\xi, s) = \frac{1}{1 + b\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{s}{(1-\alpha)s+\alpha}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{s \left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}} - 1 \right)} \frac{1 + b\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c} \right) \left(\frac{s}{(1-\alpha)s+\alpha} \right)} + \frac{\omega}{\omega^2 + s^2} \right) e^{-\xi\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{s}{(1-\alpha)s+\alpha}}} - \frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{s \left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}} - 1 \right)} \frac{e^{-\xi\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c} \right) \left(\frac{s}{(1-\alpha)s+\alpha} \right)} \quad (32)$$

Case 3. $f(t) = t \cos(t)$

In the fourth case, take $f(t) = t \cos(t)$ with its Laplace $F(q) = \frac{q^2-1}{(q^2+1)^2}$ then the expressions of velocity field by AB and CF-fractional derivative with Eqs. (21) and (28) respectively will become as

$$\bar{w}(\xi, q) = \frac{1}{1 + b\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{q^\beta}{(1-\beta)q^\beta+\beta}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta+\beta}} - 1 \right)} \frac{1 + b\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta+\beta}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c} \right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta+\beta} \right)} + \frac{q^2-1}{(1+q^2)^2} \right) e^{-\xi\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{q^\beta}{(1-\beta)q^\beta+\beta}}} - \frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta+\beta}} - 1 \right)} \frac{e^{-\xi\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta+\beta}}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c} \right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta+\beta} \right)} \quad (33)$$

and

$$\bar{w}(\xi, s) = \frac{1}{1 + b\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{s}{(1-\alpha)s+\alpha}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{s \left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}} - 1 \right)} \frac{1 + b\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c} \right) \left(\frac{s}{(1-\alpha)s+\alpha} \right)} + \frac{s^2-1}{(1+s^2)^2} \right) e^{-\xi\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{s}{(1-\alpha)s+\alpha}}} - \frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{s \left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}} - 1 \right)} \frac{e^{-\xi\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c} \right) \left(\frac{s}{(1-\alpha)s+\alpha} \right)} \quad (34)$$

Case 4. $f(t) = t e^t$

In the final case, take $f(t) = t e^t$ with its Laplace $F(q) = \frac{1}{(q-1)^2}$ then the expressions of velocity field by AB and CF-fractional derivative with Eqs. (21) and (28) respectively will become as

$$\bar{w}(\xi, q) = \frac{1}{1 + b\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{q^\beta}{(1-\beta)q^\beta+\beta}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta+\beta}} - 1 \right)} \frac{1 + b\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta+\beta}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c} \right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta+\beta} \right)} + \frac{1}{(q-1)^2} \right) e^{-\xi\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{q^\beta}{(1-\beta)q^\beta+\beta}}} - \frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta+\beta}} - 1 \right)} \frac{e^{-\xi\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{q^\beta}{(1-\beta)q^\beta+\beta}}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c} \right) \left(\frac{q^{1+\beta}}{(1-\beta)q^\beta+\beta} \right)} \quad (35)$$

and

$$\bar{w}(\xi, s) = \frac{1}{1 + b\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{s}{(1-\alpha)s+\alpha}}} \left(\frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{s\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}} - 1\right)} \frac{1 + b\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c}\right)\left(\frac{s}{(1-\alpha)s+\alpha}\right)} + \frac{1}{(s-1)^2} \right) e^{-\xi\sqrt{\frac{\Lambda_1}{\Lambda_2\beta_c} \frac{s}{(1-\alpha)s+\alpha}}} - \frac{\Lambda_3 Gr}{\Lambda_2\beta_c} \frac{1}{s\left(\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}} - 1\right)} \frac{e^{-\xi\sqrt{\frac{\Lambda_4 Pr}{\Lambda_5} \frac{s}{(1-\alpha)s+\alpha}}}}{\left(\frac{\Lambda_4 Pr}{\Lambda_5} - \frac{\Lambda_1}{\Lambda_2\beta_c}\right)\left(\frac{s}{(1-\alpha)s+\alpha}\right)} \tag{36}$$

5. Results and discussion

The main objective of this analysis is to inspect the thermal significances of graphene oxide (GO) and molybdenum disulphide (MoS₂) nanoparticles by using the Atangana-Baleanu and Caputo-Fabrizio time-fractional derivatives. The solution of partial differential governing equations is obtained by applying the Laplace scheme. The effects of different constraints on leading equations are examined graphically by using math software Mathematica and the numerical analysis of Nusselt number and skin friction is also examined. For the inverse of Laplace transformation different numerical inverse techniques, i.e. Grave Stehfest algorithm and Zakians methods are exploited. The whole analysis is performed by assigning some constants values of parameters like $\phi = 0.04$, $Pr = 1.5$, $Gr = 0.75$, $\phi = 0.04$, $h = 0.5$, $t = 0.3$, $\alpha = 0.4$, $\beta = 0.4$. Fig. 1 is sketched for the schematic analysis of flow over a surface. The effects of fractional constraint α, β and Prandtl number Pr on the temperature distribution via AB and CF fractional derivatives are examined in Fig. 2 (a) and (b) for altered values of the fractional constraint and Prandtl number Pr . The behavior of temperature profile for changed values α, β presents that temperature decays by varying the values of fractional parameters and the temperature field also decrease by varying the values of the Prandtl number. Physically, enhancement in the values of Pr decreases the thermal conductivity and increases the viciousness of the fluid due to which the temperature of the nanofluid decreases by enhancing the value of Pr . In Fig. 3(a) and (b) the possessions of volume fraction ϕ on temperature distribution and the comparison of ordinary temperature and fractional derivative (AB and CF) temperature are displayed for $\alpha, \beta \rightarrow 1$ respectively. Physically, enhancement in volume fraction values escalates the thermal conductivity which causes the addition of temperature field. While in comparison with ordinary and fractional model temperature, it overlaps on ordinary derivative when $\alpha, \beta \rightarrow 1$ in Fig. 3(b). The overlapping of curves represents the validity of our obtained results by different numerical inverse methods.

The velocity profile via AB and CF fractional derivatives for the fractional constraints α, β , and Prandtl number Pr are analyzed in Fig. 4(a) and (b). It can be seen that the velocity profile decays by variation in both parameters values fractional parameter and Prandtl number. Furthermore, the velocity profile by CF-fractional derivative decays more rapidly as compared to AB-fractional derivative and altered with the increase in time. The behavior of Grashof number Gr and volume fraction ϕ is examined for the velocity field of both fractional techniques. Variation in Grashof number causes enhancement in buoyancy effect which speed up the fluid velocity and surface slip decreases the fluid velocity as shown in Fig. 5(a–b). While variation in volume fraction varies the viscous effect of the fluid causes to addition in friction to flow and fluid slow down. The comparison of slip parameter and the comparison of the velocity field for

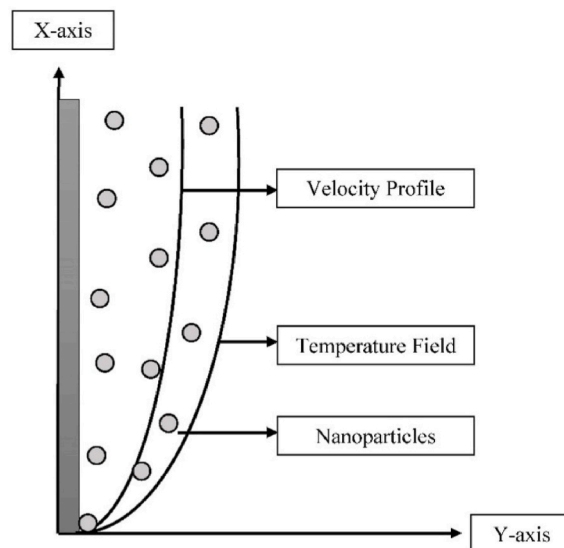


Fig. 1. Geometry of flow.

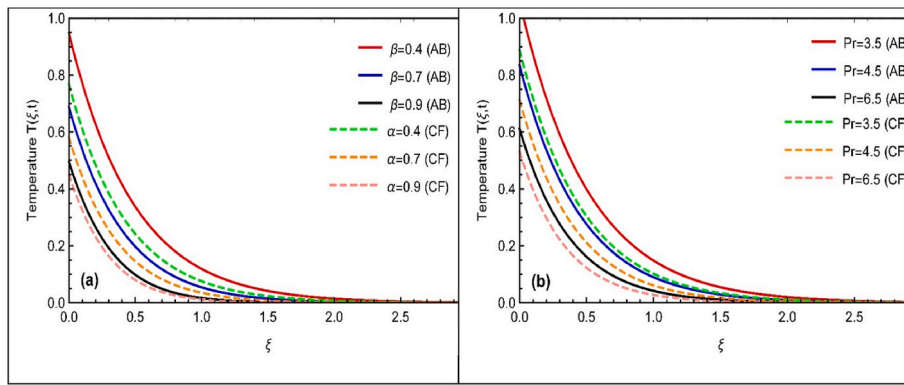


Fig. 2. (a–b):Temperature field with the variation in (a):fractional constraint α, β and (b):Prandtl number with $\phi = 0.04, Pr = 1.5, t = 0.3$.

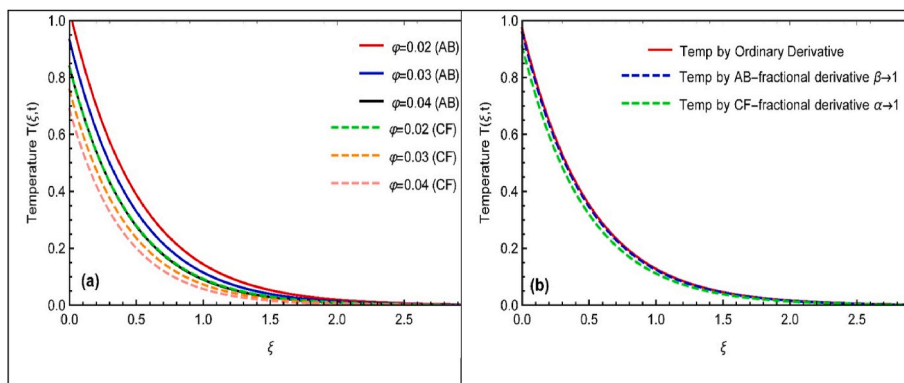


Fig. 3. (a–b):Temperature field with the variation in (a)volume fraction and (b):comparison with ordinary temperature.

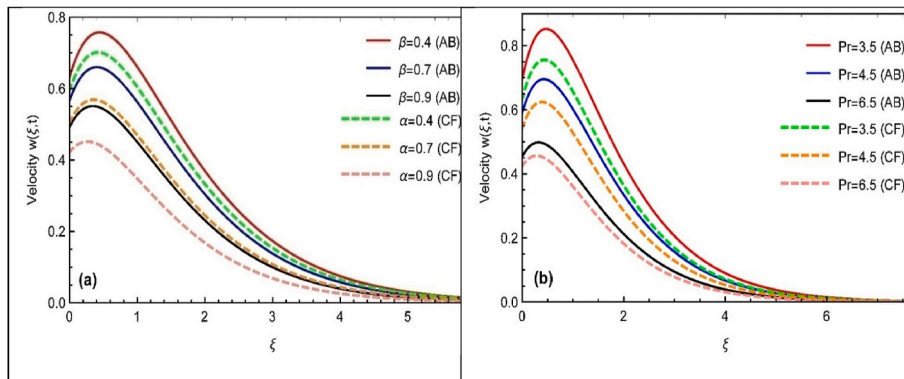


Fig. 4. (a–b):Velocity field with variation in (a): fractional constraint α, β and (b):Prandtl number with $h = 0.5, Gr = 0.75, \phi = 0.04, t = 0.3$.

different nanoparticles is analyzed in Fig. 6(a) and (b) respectively. The velocity of CF-time fractional derivative relatively more decays as compared to AB-time fractional derivative model velocity. Furthermore, the velocity of (MoS_2)based nanoparticles more decay as compared to (GO)based nanoparticles. Finally, the comparison of numerical techniques namely the Stehfest and Zakians method and the comparison of fractional model velocity with ordinary derivative model velocity is plotted in Fig. 7(a) and (b) respectively. It is seen that the curves of both numerical techniques overlap each other which proves the validity of obtained results. When the values of fractional parameter tend to be 1 then the curves of both fractional models overlap to ordinary velocity model which also signifies the validation of velocity profile results. Table 2 presents the variations in Nusselt number against α and. A lower change is heat transfer rate is noted for both parameters. Table 3 predicts the variation of skin friction coefficient for α, β at different time instants. The numerical simulations are performed for both Atangana-Baleanu (AB) and Caputo-Fabrizio (CF) derivatives. With increasing α and β ,

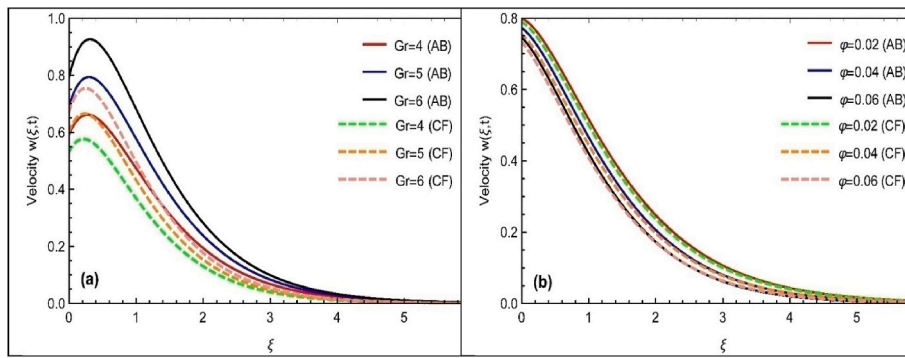


Fig. 5. (a–b): Velocity field with variation in (a):Grashof number and (b):volume fraction with $\alpha, \beta = 0.5, h = 0.5, Pr = 1.5, t = 0.3$.

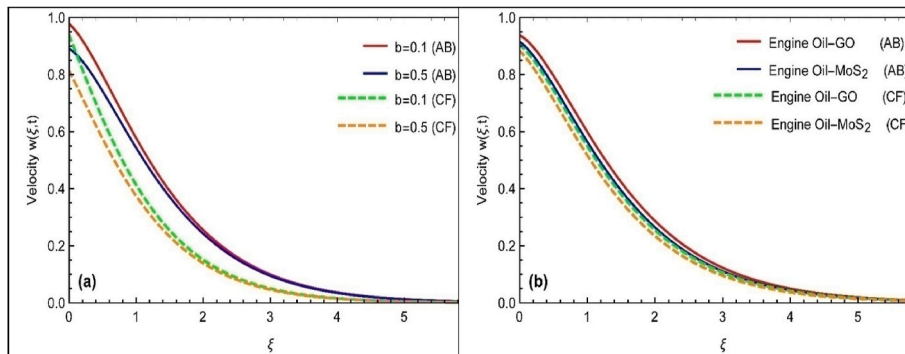


Fig. 6. (a–b): Velocity field with variation in (a): slip parameter and (b): comparison of nanoparticles.

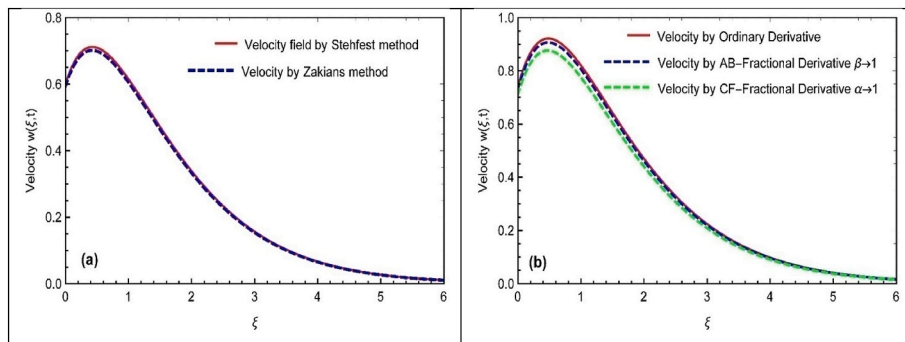


Fig. 7. (a–b): Velocity field with(a):comparison of numerical methods and (b):comparison with the ordinary velocity.

Table 3

Analysis of skin friction C_f with variation in the fractional parameter at different times by AB and CF fractional derivative.

α, β	$C_f (AB) t = 1.2$	$C_f (CF) t = 1.2$	$C_f (AB) t = 1.5$	$C_f (CF) t = 1.5$	$C_f (AB) t = 1.7$	$C_f (CF) t = 1.7$
0.1	0.5836	0.6146	0.6518	0.6284	0.6430	0.5962
0.2	0.5709	0.6100	0.6275	0.6000	0.6110	0.5414
0.3	0.5560	0.6082	0.5924	0.5736	0.5623	0.4879
0.4	0.5439	0.6070	0.5515	0.5470	0.5015	0.4335
0.5	0.5387	0.6038	0.5094	0.5174	0.4334	0.3755
0.6	0.5420	0.5956	0.4688	0.4819	0.3612	0.3118
0.7	0.5521	0.5786	0.4293	0.4378	0.2859	0.2412
0.8	0.5634	0.5501	0.3867	0.3846	0.2053	0.1654
0.9	0.5655	0.5115	0.3344	0.3265	0.1165	0.0903

the numerical values of skin friction coefficient get declining trend.

6. Concluding remarks

The thermal properties of graphene oxide (GO) and molybdenum disulphide (MoS_2) nanoparticles have been discussed with help of fractional derivative approach. The engine oil is assumed as a base fluid for which the thermal performances are improved. The Atangana-Baleanu (AB) and Caputo-Fabrizio (CF) derivatives are followed to presents the numerical simulations. The accuracy of both schemes is verified. The main findings are:

- A decreasing change in the heat transfer rate is observed for the fractional parameters.
- The velocity profile improves with Grashof number while reverse velocity change has been noticed for fractional parameters.
- The temperature and velocity field of fractional model about overlaps to ordinary derivative model for $\alpha, \beta \rightarrow 1$.
- The nanoparticles temperature reduces with volume fraction coefficient.
- The profile of velocity simulated for AB-fractional model is relatively progressive as compared to CF-fractional model.
- The velocity profile of molybdenum disulphide based nanoparticles is a relatively greater than graphene oxide nanoparticles.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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